## **M1.**(a) (i) Appreciates pV should be constant for isothermal change (by working or statement) $W = p\Delta V$ is TO

Allow only products seen where are approximately 150 for 1 mark Penalise J as unit here

M1

Demonstrates pV = constant using 2 points (on the line) set equal to each other or conclusion made or **shows** that for V doubling that p halves (worth 2 marks)

need to see values for p and V

Products should equal 150 to 2 sf Accept statement that products are slightly different so not quite isothermal

Α1

Demonstrates pV = constant using 3 points (on the line) with conclusion Need to see values for p and V

> Products should equal 150 to 2 sf Accept statement that products are slightly different so not quite isothermal

> > **A1**

3

(ii) Adiabatic <u>therefore</u> no heat transfer **or** Adiabatic therefore Q = 0

B1

Work is done by gas therefore W is negative or Work is done by gas therefore energy is removed from the system

В1

<u>AU</u> is negative <u>therefore</u> internal energy of gas decreases **or** energy is removed from the system <u>therefore</u> internal energy of gas decreases or work done by the gas <u>so</u> internal energy decreases

Allow

$$-\Delta U = -W \text{ or } \Delta U = -W$$

**B**1

3

(iii) Uses 
$$pV/T$$
 = constant or uses  $pV$ = $nRT$  or uses  $pV$ = $NkT$  e.g. makes  $T$  subject or substitutes into an equation with  $p_A$  and  $V_A$  or  $p_C$  and  $V_C$  (condone use of n = 1) or 
$$\frac{(pV)_A}{(pV)_C}$$
 their 
$$\frac{(pV)_A}{(pV)_C}$$
 
$$V_a \ read \ off \ range$$
 = 2.5 to 2.6 (× 10<sup>-4</sup>) 
$$p_A$$
 = 600 × 10<sup>3</sup> 
$$V_C \ read \ off \ range$$
 = 8.5 to 8.6 (× 10<sup>-4</sup>) 
$$p_C$$
 = 140 × 10<sup>3</sup>

C1

Correct substitution of coordinates (inside range) into  $\frac{(pV)_{\rm A}}{(pV)_{\rm C}}$ 

With consistent use of powers of 10

 $(pV)_{\scriptscriptstyle A}$  range is 150 to 156 and  $(pV)_{\scriptscriptstyle C}$  range is 119 to 120.4

C1

1.2(5) Allow range from 1.2 to 1.3

Accept decimal fraction: 1

Α1

3

(b) Energy per large square = 10(J) or states that work done is equal to area under curve (between A and B)
 or energy per small square = 0.4(J)
 or square counting seen on correct area

Must be clear that area represents energy either by subject of formula or use of units on 10 or 0.4

Alternative: W = area of a trapezium (with working)  $\mathbf{or} \ W = P_{\text{mean}} \times \Delta V \ \mathbf{or}$   $W = 450 \times 10^3 \times 2.5 \times 10^{-4}$   $\mathbf{or} \ W = \text{area of a rectangle} + \text{area of a triangle (with working)}$ 

Number of large squares = 10.5 to 11.5 seen <u>and</u> (W) = number of squares × area of one square (using numbers) Range = 105 to 115 (J) Or

Number of small squares = 263 to 287 seen  $\underline{and}$  (W) = number of squares × area of one square (using numbers) Range = 105 to 115 (J)

States that actual work done would be lower because of curvature of line

B1

2

(c) (Total energy removed per s =) 4560 (J) or number of cycles per s = 40 or (Mass per second =) 114  $\div$  68400 in rearranged form or their energy  $\div$  (c  $\Delta T$ ) or their energy  $\div$  68400

C1

0.067 (kg) seen Allow 0.066 (kg) here or allow V / t = 1.67 ×  $10^{-3} \div 1100$  or  $(\frac{V}{t}) = \frac{E}{\rho c \Delta \theta}$  and correct substitution seen

Condone E = 114 (J) **or** temperature = 291(K)

C1

=  $0.061 \times 10^{-3}$  or  $6.06 \times 10^{-5}$  (m<sup>3</sup>)

A1

[14]

3

**M2.**(a) (i) Clear statement that for isothermal pV =constant or  $p_1V_1 = p_2V_2$   $\checkmark$  Applies this to any 2 points on the curve AB  $\checkmark$  e.g.  $1.0 \times 10^5 \times 1.2 \times 10^{-3} = 4.8 \times 10^5 \times 0.25 \times 10^{-3}$  120 = 120 Allow pV = c applied to intermediate points **estimated** from graph e.g.  $V = 0.39 \times 10^{-3}$ ,  $p = 3 \times 10^5$ 

2

(ii) 
$$W = p \Delta v$$
  
=  $4.8 \times 10^{5} \times (0.39 - 0.25) \times 10^{-3}$   
=  $67 J \checkmark$ 

1

(b)

	Q/J	W/J	ΔU/J	
process $A \rightarrow B$	-188	-188	0	\ \
process $B \rightarrow C$	+235	(+)67	(+)168	/
process $C \rightarrow A$	0	+168	-168	/
whole cycle	+47	+47	0	/

Any horiz line correct up to max 3 Give CE in  $B \rightarrow C$  if ans to ii used for W If no sign take as +ve

max 3

(c) 
$$\eta_{overall} = 47 / 235 = 0.20 \text{ or } 20\%$$

1

 (d) Isothermal process would require engine to run very slowly / be made of material of high heat conductivity ✓
 Adiabatic process has to occur very rapidly / require perfectly insulating

Adiabatic process has to occur very rapidly / require perfectly insulating container / has no heat transfer <

Very difficult to meet both requirements in the same device Very difficult to arrange for heating to stop exactly in the right place (C) so that at end of expansion the curve meets the isothermal at A

> Do not credit bald statement to effect adiabatic / isothermal process not possible - must give reason

Ignore mention of valves opening / closing, rounded corners, friction, induction / exhaust strokes wtte

max 2

[9]

M3. (a) (i) Indicated work per cylinder = area of loop √ [either stated explicitly or shown on the Figure e.g. by shading or ticking squares or subsequent correct working.]

appropriate method for finding area e.g. counting squares  $\checkmark$  correct scaling factor used [to give answer of 470 J  $\pm$  50 J]  $\checkmark$  indicated power =  $4 \times 0.5 \times (4100/60) \times 470$ 

= 64 kW √

(ii) (Fuel flow rate = 0.376/100 = 0.00376 litre s<sup>-1</sup>)

Input power (= c.v. × fuel flow rate)

(= 145 kW)

Π overall = brake power/input power ✓ seen or implied from correct subsequent working

$$= 55.0/145 = 0.38 \text{ or } 38\%$$

3

(b) Power expended in overcoming friction
 in (all) the bearings / between piston & cylinder ✓
 and / or in circulating oil / cooling water ✓
 and / or driving auxiliaries (e.g. fuel injection pump) ✓

1

1

(c) Represents the induction <u>and</u> exhaust (strokes) (which take place at nearly atmospheric pressure). ✓

[9]

**M4.** (a) (i) work done (per kg) = area enclosed (by loop) (1) suitable method of finding area (e.g. counting squares) (1)

(ii) 
$$P$$
 (= work done per kg x fuel flow rate)  
= 500 (kJ) × 9.9 (kgs<sup>1</sup>) = 5000kW (1)  
(4950kW)

(iii) (output power = indicated power - friction power)
$$P_{out} = 4950 - 430 = 45(20) \text{ kW (1)}$$
(use of  $P = 5000 \text{ gives } P_{out} = 45(70) \text{kW}$ )
(allow C.E. for values of  $P$  in (ii))

(b) (i)  $P_{in}$  (= fuel flow rate × calorific value) =  $0.30 \times 44 \times 10^{\circ} = 13(.2) \times 10^{\circ}W$  (1)

efficiency = 
$$\frac{4520 \times 10^{3}}{13.2 \times 10^{6}}$$
 = 34% (1) (allow C.E. for value of  $P_{out}$  in (a) (iii) and  $P_{in}$  in (b) (i))

5

2

2

[7]

**M5.** (a) 
$$T_H = 273 + 820 = 1093$$
 (K),  $T_C = 273 + 77 = 350$  (K) (1)

efficiency = 
$$\frac{T_H - T_C}{T_H} = \frac{1093 - 350}{1093} = 0.68 \text{ or } 68\% \text{ (1)}$$

(b) rotational speed of output shaft =  $\frac{1800}{2 \times 60}$  = 15 rev s<sup>-1</sup> (1) (work output each cycle = 380 J, 2 rev = 1 cycle in a 4 stroke engine)

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indicated power = 
$$15 \times 190 = 5.7 \text{ kW (1)}$$

(d) energy supplied per sec (= fuel flow rate x calorific value)

$$= \frac{2.1 \times 10^{-2}}{60} \times 45 \times 10^{6} = 16 \text{ kW (15.8 kW) (1)}$$

(e) efficiency = 
$$\frac{\text{net power output}}{\text{power input}} = \frac{4.7}{16} = 0.29 \text{ or } 29 \%$$

$$\frac{4.7}{15.8}$$
 = 0.30 or 30%

(allow C.E. for value from (d))

[7]

2

1

1